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Very high cycle fatigue of a high strength steel under sea water corrosion: A strong corrosion and mechanical damage coupling

Ruben Pérez-Mora^a, Thierry Palin-Luc^{b,*}, Claude Bathias^a, Paul C. Paris^c

^a Université Paris Ouest, LEME, 50 rue de Sevres, 92410 Ville d'Avray, France

^b Arts et Metiers ParisTech, I2M, CNRS, Université de Bordeaux, Esplanade des Arts et Metiers, 33405 Talence Cedex, France

^c Parks College of Engineering, Aviation and Technology, St. Louis University, St. Louis, MO 63103, USA

A B S T R A C T

This paper is focused on the effect of sea water corrosion on the gigacycle fatigue strength of a martensitic–bainitic hot rolled steel R5 used for manufacturing off-shore mooring chains for petroleum platforms in the North Sea. Crack initiation fatigue tests in the regime of 10^6 to 10^{10} cycles were carried out on smooth specimens under three different environment conditions: (i) without any corrosion (virgin state) in air, (ii) in air after pre-corrosion, and (iii) in-situ corrosion-fatigue under artificial sea water flow. A drastic effect of sea water corrosion was found: the median fatigue strength beyond 10^8 cycles is divided by 5 compared to virgin state specimens. The crack initiation sites were corrosion pits caused by pre-corrosion or created during corrosion-fatigue under sea water flow. Furthermore some sub-surface and internal crack initiations were observed on specimens without any corrosion (virgin state). Crack propagation curves were obtained in mode I in air and under sea water flow. Calculation of the stress intensity factor at the tip of cracks emanating from hemispherical surface pits combined with the Paris–Hertzberg–Mc Clintock crack growth rate model showed that fatigue crack initiation period represents most of the fatigue life in the VHCF regime. Additional original experiments have shown physical evidences that the fatigue strength in the gigacycle regime under sea water flow is mainly governed by the corrosion process with a strong coupling between cyclic loading and corrosion.

Keywords:

Gigacycle fatigue

Corrosion

Steel

Crack initiation

Crack growth

1. Introduction

The mooring chains of off-shore petroleum platforms are designed for 30 years and loaded in fatigue in corrosive environment due to sea water. Because of the ocean waves (frequency varying between 0.1 and 1 Hz) 24 h a day, the number of load cycles during 30 years is between 9.5×10^7 and 9.5×10^8 cycles that is in the gigacycle regime (more than 10^8 cycles). This study is focused on the gigacycle fatigue strength of low alloy steel used for manufacturing such chains. The effect of pre-corrosion and real time corrosion conditions on the fatigue strength and crack growth rate are investigated. It has been demonstrated by many studies on steel and aluminum alloys in the gigacycle regime that there is no fatigue limit for such metals beyond 10^7 cycles as was believed in the past [1,2]. Moreover, fatigue cracks initiate mainly at surface defects in the short fatigue life regime, but may shift to subsurface in the long life range [3]. Some other studies have shown that defects like non-metallic inclusions, pores [4] or pits [5–7] are

the key factors that control the fatigue behavior of metals in very high cycle fatigue (VHCF) regime. On the other hand, some studies have been proving that crack initiation dominates the total fatigue life of iron alloys in gigacycle fatigue in air [8,9]. Furthermore, the influence of static deformation has been studied confirming that both passive and transpassive current densities on stainless steel reach a maximum in the course of growing plastic strain [10]. Other studies have investigated the dissolution under chemical products on stainless steel with active, passive and intermediate potentials where it is presumed that dissolution is enhanced during cyclic loading [11]. But the effect of aqueous corrosion on the fatigue strength with regard to crack initiation in the VHCF regime is not very much studied in literature [12]. In this regime the material is loaded in its elastic domain at the macroscopic scale. In this study the effect of sea water corrosion (under free potential) on the VHCF strength is studied.

After presenting the investigated material and the experimental conditions both for crack initiation and crack propagation tests, experimental results are presented and discussed with regard to SEM observations of the fracture surface. It is shown that a drastic effect of sea water corrosion decreases the fatigue strength of the

* Corresponding author.

E-mail address: thierry.palin-luc@ensam.eu (T. Palin-Luc).

Nomenclature

a	crack length	N_{ao-ai}	number of cycles of the small crack growth period
a_{int}	crack length at initiation	$N_{aint-ao}$	number of cycles of the short crack growth period
a_0	crack length at the corner of the crack growth curve corresponding to the threshold ΔK_{th}	R	radius of hemispherical surface defect
b	Burger vector	U_0	displacement amplitude at the extremity of the specimen
E	Young's modulus	w	width of the crack growth specimen
N_f	total number of cycles to failure including initiation and propagation periods	ν	Poisson ratio
N_{prop}	number of cycles of the crack propagation period	ΔK	range of the stress intensity factor
N_{ai-a}	number of cycles of the long crack growth period	ΔK_{th}	range of the stress intensity factor at the threshold
		σ_a	stress amplitude

steel under sea water flow. The assessment of the crack growth helps us to show that crack initiation dominates the total fatigue life in the gigacycle regime. Furthermore, additional experiments allow the authors to show experimental evidences of coupling between corrosion and cyclic loading even under ultrasonic load-frequency.

2. Material and experimental conditions

The material studied hereafter is a non-standard hot rolled low alloy steel grade (named R5 according to the International Classification Societies of Off-shore Systems) with a typical fine grain microstructure, composed by tempered martensite and bainite, as shown in Fig. 1. Its chemical composition is shown in Table 1. This steel is used after a double quenching in water, a first period at 920 °C and a second period at 880 °C and then tempering at 650 °C with water cooling. After this heat treatment its mechanical properties are: hardness 317 HB, yield strength 970 MPa, ultimate tensile strength UTS = 1018 MPa, Young modulus $E = 211$ GPa under monotonic quasi-static tension. It has to be noticed that this steel is vacuum degassed with low hydrogen content (1 ppm maximum in the liquid steel after the vacuum treatment). Furthermore, very low non-metallic inclusions are present in this steel (see details in [12]).

2.1. Fatigue test conditions and specimen geometry

2.1.1. Testing machine and specimen geometry

All the fatigue tests (crack initiation and crack growth) presented hereafter were carried out with an ultrasonic fatigue testing

Table 1
Composition of R5 steel (wt%, Fe balance).

C	Mn	Si	P	S	Cr	Ni	Mo	V	O
0.22	1.22	0.3	0.009	0.003	1.07	1.07	0.5	0.09	12 ppm

machine [1] operating continuously at 20 kHz (no pulse loading) under fully reversed tension ($R = -1$) (see [1,12] for details). Fig. 2 shows the dimensions of the two types of specimens used for (a) VHCF crack initiation tests and (b) fatigue crack growth (FCG) tests. The geometry of the FCG specimens was designed according to the works of Wu [13] and Sun [14]. The crack growth was measured with an optical binocular microscope equipped with a digital camera; this set up has a maximum magnification $\times 200$ and a resolution of 0.5 μm . The roughness of the tested area of the VHCF specimens was $Ra = 0.6 \mu\text{m}$; additionally a few specimens with a lower arithmetic roughness ($Ra = 0.1 \mu\text{m}$) were tested too for investigating the effect of roughness. The VHCF specimens were tested under three different conditions: (i) without any corrosion (virgin state), (ii) after pre-corrosion and (iii) under real time artificial sea water flow.

All the VHCF tests were calibrated by using a wide band (100 kHz) strain gauge conditioner and a longitudinal strain gauge glued on the specimen surface. Such calibration allows the authors to be certain of the local strain (elastic stress) amplitude and mean value in the narrowest cross section of the specimen. These tests were carried out until a decrease of the resonance frequency of 0.5 kHz that indicates the presence of a macrocrack.

2.1.2. Corrosion of the specimens

The pre-corrosion of the specimens was done according to the ASTM G85 standard: 600 h in a salt fog corrosion chamber under temperature and humidity control (35 °C with 95% of humidity). The salt solution contains 5% of NaCl, its pH was 6.6 and it was applied in the chamber with a flow rate of 1.52 ml/h. After the pre-corrosion process the specimens were first chemically cleaned and then cleaned with emery paper to remove the oxide layer. Many corrosion pits were created by the salt fog (Fig. 3) which diameter is between 30 and 80 μm . These pits have hemispherical shape and their depth can be compared with their radius. Comparing this dimension to prior austenite grain size, the pits are in between one and two times the size of the prior austenite grains.

To carry out VHCF tests in sea water environment a special corrosion cell was designed (see [12] for details). To avoid any cavitation it was decided to test the specimens under sea water flow without immersion. This is representative of the splash zone of the mooring chains. To do that a peristaltic pump creates a flow of sea water (100 ml/min) on two opposite sides of the specimen surface in the tested area (diameter 3 mm). The sea water used was the A3 standard synthetic sea water; its chemical composition

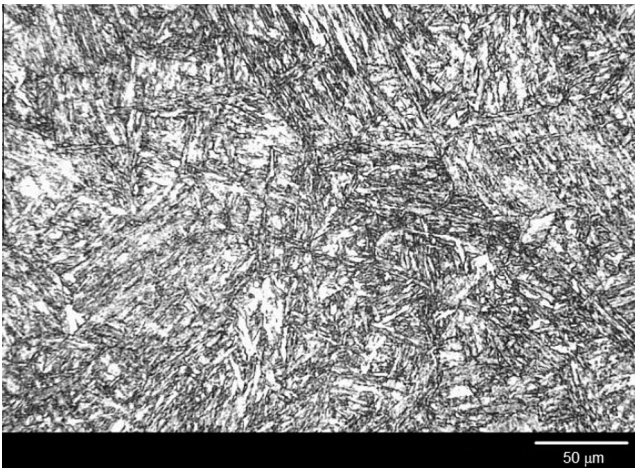


Fig. 1. R5 steel microstructure (after Nital etching 2%).

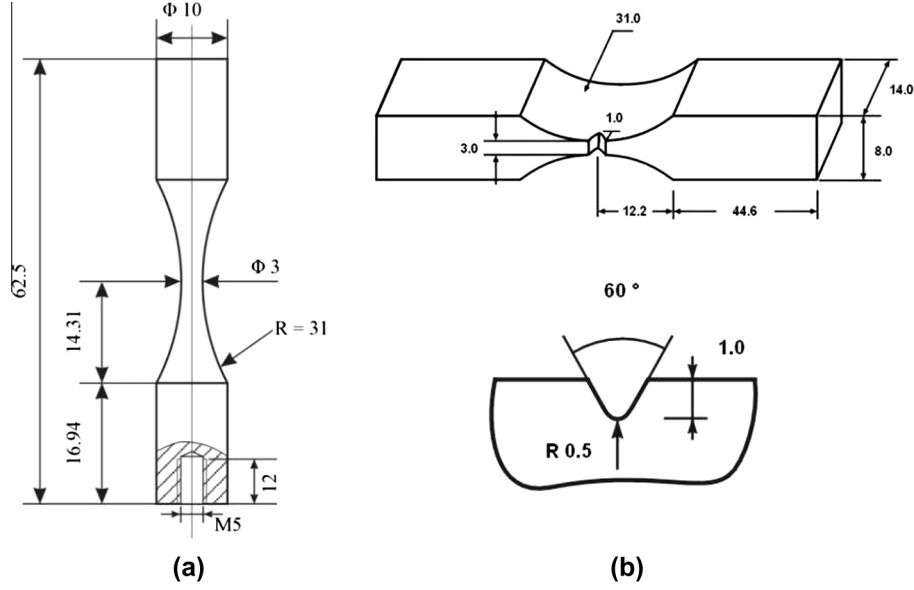


Fig. 2. Specimen geometry for (a) VHCF tests, $K_t = 1.02$, (b) crack growth tests (dimensions in mm).

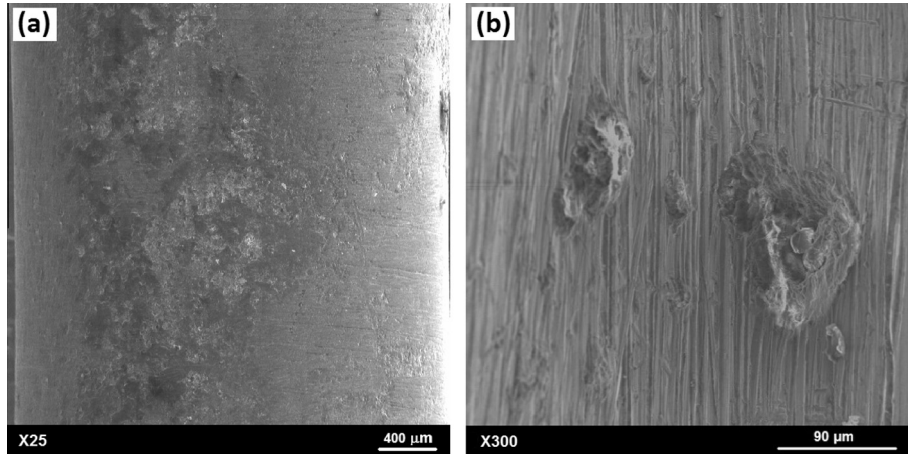


Fig. 3. (a) Surface of a specimen after pre-corrosion in the salt fog chamber, (b) zoom on a corrosion pit.

(in weight) is: 24.53% NaCl, 5.2% $MgCl_2$, 4.09% Na_2SO_4 , 1.16% $CaCl_2$, 0.695% KCl and 0.201% $NaHCO_3$. The pH of this solution is 6.6 and specimens were tested under free potential. The temperature of the sea water was 20–25 °C (room temperature).

2.1.3. Fatigue crack growth tests

Fatigue crack growth tests were carried out under fully reversed tension ($R = -1$) in mode I following a similar methodology than prescribed in ASTM E647 standard. Since with the ultrasonic fatigue testing device the specimen is loaded under displacement control, the range of the mode I stress intensity factor ΔK was computed according to Refs. [13,14]:

$$\Delta K = U_o \left(\frac{E}{1 - \nu^2} \right) \sqrt{\frac{\pi}{a}} Y(a/w) \quad (1)$$

where

$$Y(a/w) = 0.635(a/w) + 1.731(a/w)^2 - 3.979(a/w)^3 + 1.963(a/w)^4.$$

U_o is the displacement amplitude imposed at the top of the specimen by the horn of the ultrasonic machine, E is the dynamic modulus and ν is the Poisson ratio of the material, $Y(a/w)$ is a function depending on the specimen geometry, w is the width of the

specimen and a is the crack length measured from the specimen surface (i.e. including the notch depth of 1 mm). A natural pre-crack of 0.5 mm (from the notch root) is developed in tension-compression before the crack growth test itself. For the crack growth tests carried out in sea water the pre-crack was done in air and then the specimen with the natural crack at the notch was tested.

3. Experimental results and discussion

3.1. Fatigue crack initiation tests

Fig. 4 shows the S-N curves up to fracture. The scatter of the fatigue strength is larger for the pre-corroded specimens than for the virgin ones (45.7 and 18.2 MPa respectively). However a decreasing of around 50 MPa of the fatigue strength for the specimens with pre-corrosion is observed compared to the specimens without any corrosion. There is a drastic effect of sea water flow on the fatigue strength of the R5 steel in the VHCF fatigue regime. Indeed, for the specimens tested under sea water flow, the fatigue strength at 10^7 cycles is around 300 MPa, not far from the value for

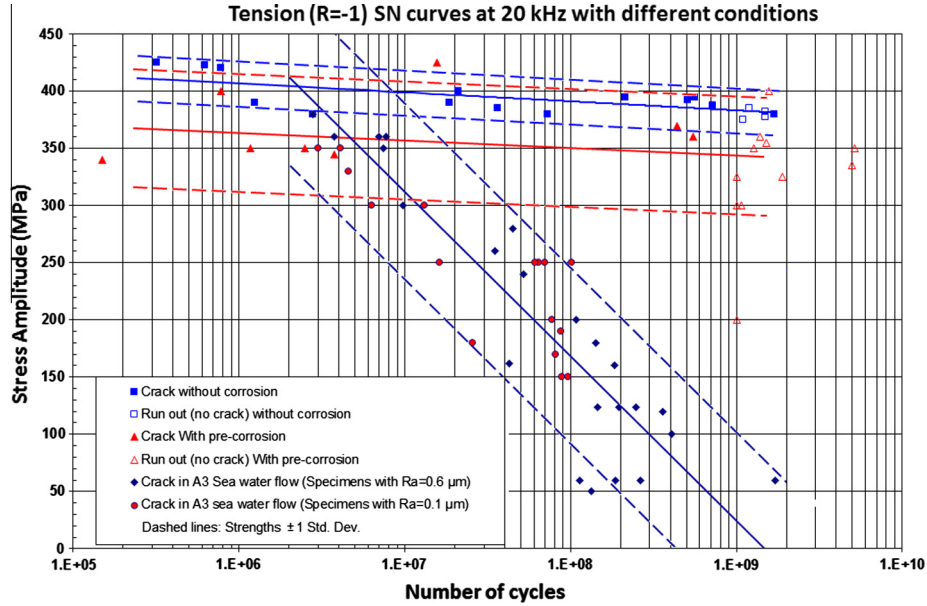


Fig. 4. S-N curves of the R5 steel under fully reversed tension at 20 kHz.

pre-corroded specimens (360 MPa), but for 3×10^8 cycles the fatigue strength is around 100 MPa only. That is a decrease of 74% compared to the non-corroded specimens (390 MPa) and a decrease of 71% compared to the pre-corroded ones (350 MPa). This shows that stopping the fatigue tests at 10^7 cycles and then extrapolating the S-N curve may lead to a large overestimation of the corrosion-fatigue resistance.

The fatigue tests were carried out at 20 kHz under corrosive environment and may be seen first as non-representative experiments because of the high loading frequency compared with the characteristic time of the corrosion process. However, it has been shown by El May et al. [18] that the fatigue strength in tension of a martensitic stainless steel in the high cycle fatigue regime (at 10^7 cycles) is significantly reduced by corrosion in 0.1 M NaCl aqueous solution even at 120 Hz. Furthermore, these authors have shown that there is no significant frequency effect between 10 and 120 Hz between 10^5 and 10^7 cycles.

Our fatigue corrosion tests results (Fig. 4) show that the S-N curve of specimens tested under sea water flow crosses (around $2-3 \times 10^6$ cycles) the S-N curve of virgin specimens (tested in air without any corrosion). This is not in agreement with a frequency effect but with the fact that a number of cyclic reversals ($2 \times N$) are needed to create corrosion fatigue defects and coupling as proposed in [18]. This will be discussed later in this paper.

3.2. SEM observation of the fracture surfaces

On virgin specimens, even if some unusual internal crack initiations were observed (Fig. 5), most of the fatigue cracks initiated at the specimen surface over the cycle range (10^6-10^9 cycles). But for this set of specimens no defect was observed in the crack initiation area. Surface corrosion pits were the origins of the cracks for both pre-corroded specimens and specimens tested under sea water flow (Figs. 6 and 7). For the specimens tested under sea water flow the cracks initiated all around the specimen surface due to several large corrosion pits. The size of the pits depends on the time (i.e. the number of cycles); their diameter is smaller on the pre-corroded specimens (30–80 μm) than under sea water flow (50–300 μm) (Figs. 6 and 7). Furthermore, a lot of small cracks, perpendicular to the loading direction (mode I), were observed at

the surface of the specimens tested under sea water flow, as shown in Fig. 7(c); whereas such small cracks were not observed on both virgin and pre-corroded specimens. This is characteristic of a corrosion/cyclic loading interaction.

Since a significant decrease of the fatigue strength has been observed due to corrosion pits (seen as geometrical defects), it is important to determine if the crack propagation stage dominates the total fatigue life.

3.3. Assessment of the crack initiation and propagation duration

The experimental $\frac{da}{dN} = f(\Delta K)$ curve is shown in Annex 1; this is re-plotted as $\frac{da}{dN} = f\left(\frac{\Delta K_{\text{eff}}}{E\sqrt{b}}\right)$ curve in Fig. 8. This shows that in air the mode I stress intensity factor threshold for R5 steel is around $3.3 \text{ MPa}\sqrt{\text{m}}$ for ($R = -1$). This value is between 2 and $10 \text{ MPa}\sqrt{\text{m}}$ as reported for steels in Refs. [22,23]. As usual the crack growth rate is faster under sea water flow than in air [15]. The fatigue crack propagation duration was assessed according to the work of Paris et al. [8,9], based on the Paris-Hertzberg-Mc Clintock crack growth model: $\frac{da}{dN} = b\left(\frac{\Delta K_{\text{eff}}}{E\sqrt{b}}\right)^3$ and $\left(\frac{K_{\text{eff}}}{E\sqrt{b}}\right) = 1$ at the corner (intersection between the Paris line and the threshold line), where E is the elastic modulus and b is the Burger's vector. The good agreement of this equation with our experimental data and $b = 0.285 \text{ nm}$ was shown in [12]. Since in our experiments at 20 kHz the measurement of K_{op} is not possible, in first approximation $\Delta K_{\text{eff}} \approx K_{\text{max}}$ was assumed. We do not know if K_{op} is frequency dependent that is why its value was not measured at low frequency and assumed to be the same at 20 kHz. Furthermore the authors assume that water present into the crack does not modify the value of the stress intensity factor. It is clear in Fig. 8 that since the crack growth rate in sea water is higher than in air; computing the crack growth duration based on the crack growth curve in air may only underestimate this duration.

To assess this duration, a corrosion pit was not modeled as a crack-like defect but it was modeled as a hemispherical surface defect of radius R with a semi-circular crack emanating from it. The existence of these hemispherical pits was observed by scanning electron microscopy on the surface of different specimens with pre-corrosion in salt fog chamber (Fig. 3) and after corrosion

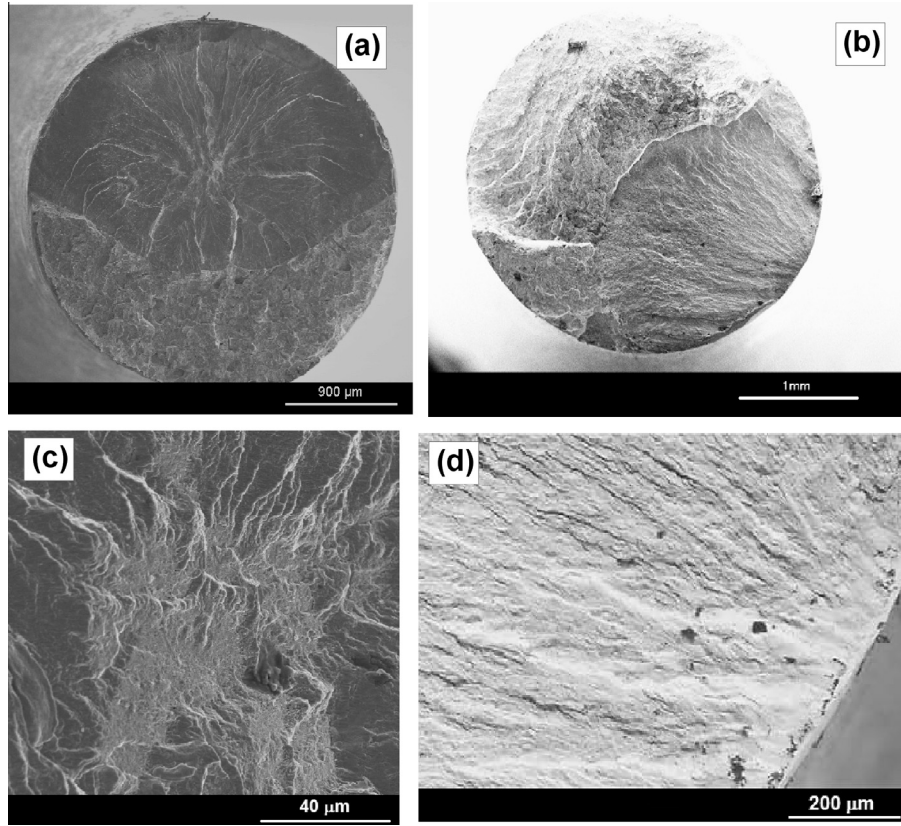


Fig. 5. Fracture surface of R5 steel virgin specimens (a, c) internal crack initiation $\sigma_a = 380$ MPa, $N_f = 2.78 \times 10^6$ cycles, (b, d) surface crack initiation $\sigma_a = 395$ MPa, $N_f = 5.61 \times 10^8$ cycles.

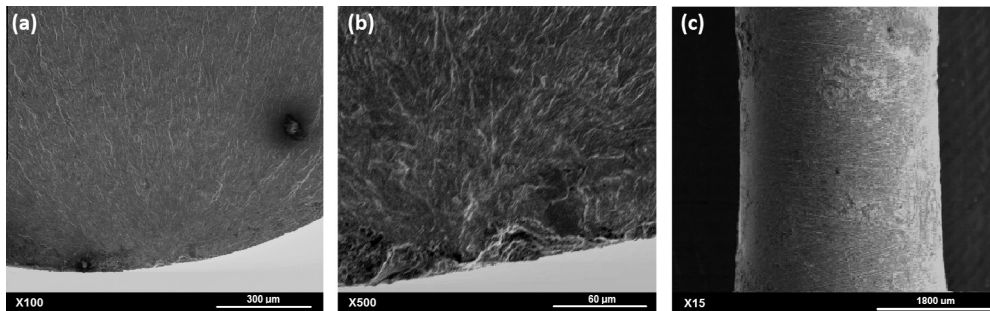


Fig. 6. Specimen with pre-corrosion, $\sigma_a = 425$ MPa, $N_f = 1.6 \times 10^7$ cycles.

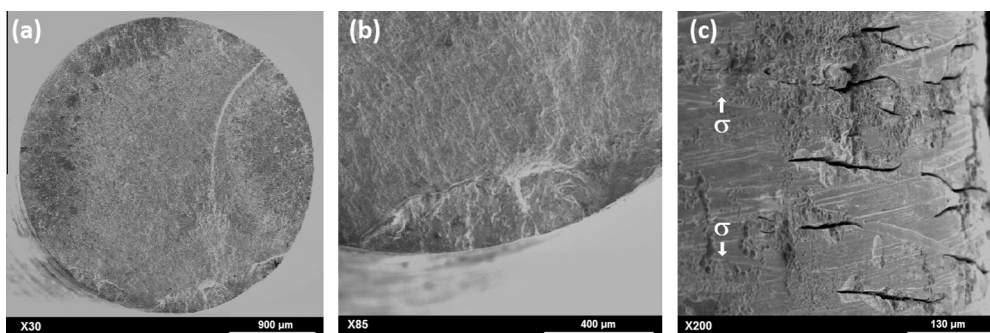


Fig. 7. Specimen tested under sea water flow, $\sigma_a = 240$ MPa, $N_f = 5.2 \times 10^7$ cycles.

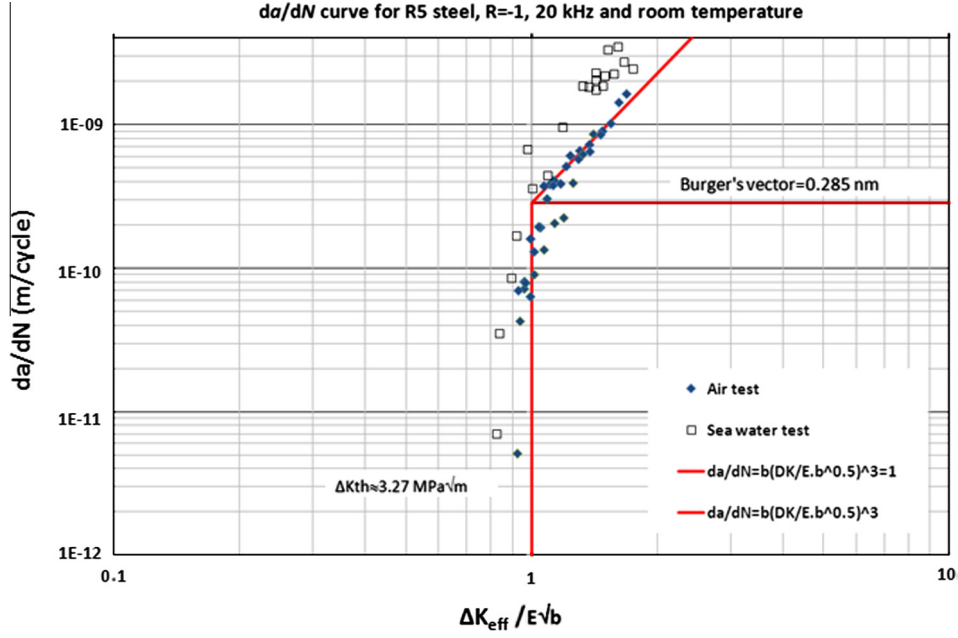


Fig. 8. $\frac{da}{dN} = f\left(\frac{\Delta K_{eff}}{E\sqrt{b}}\right)$ curve in mode I for the R5 steel ($R = -1$), in air and under sea water flow at room temperature.

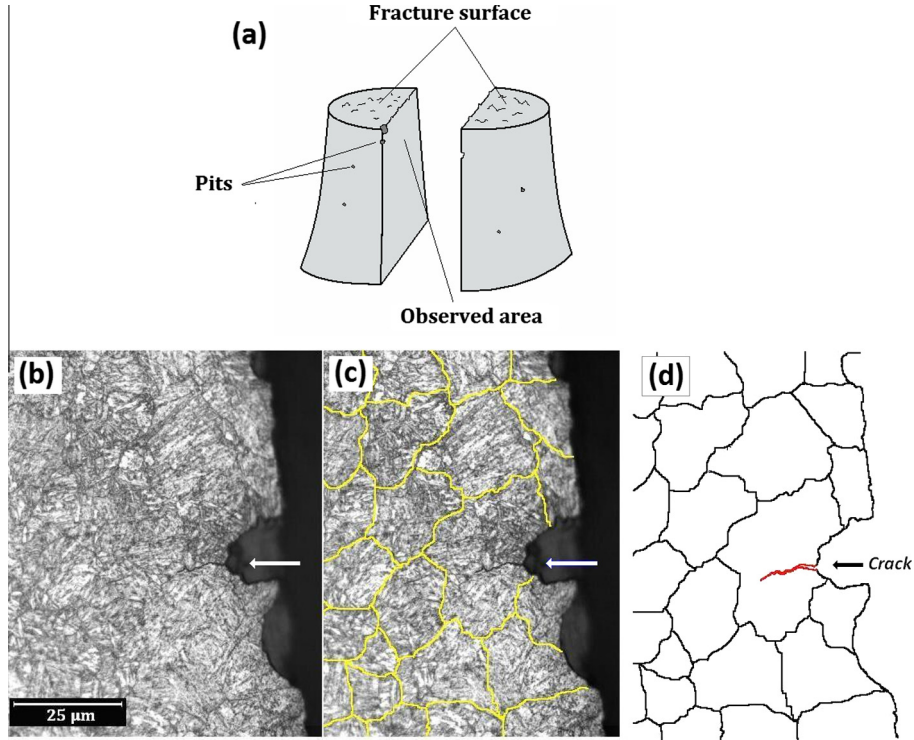


Fig. 9. Longitudinal cross section of a specimen as: (a) the sketch, showing (b) a fatigue crack initiation at a corrosion pit, (c) the old austenitic grains are yellow highlighted, (d) illustration of the short fatigue crack and the grain boundaries.

under A3 sea water flow (Fig. 7). The longitudinal cross section of a pre-corroded specimen (after 4.37×10^8 cycles under a stress amplitude of 370 MPa) close to the fracture surface was observed as illustrated in Fig. 9(a) and (b). This shows a short crack initiated at a corrosion pit. Based on this observation, an initial fatigue crack of depth a_{int} emanating from the surface of the hemispherical pit and perpendicular to the loading direction due to intercrystalline corrosion cracking was assumed. The length of the initial short

crack emanating from hemispherical defects was assumed to be $a_{int} \sim 10 \mu\text{m}$ (Fig. 9(c) and (d)).

According to the asymptotic approximation proposed by Paris et al. [16] (with details in [24]) the crack tip stress intensity factor in mode I is: $K_I = \sigma Y(x/v) \sqrt{\pi a}$, where $x = a/R$, v is the Poisson ratio, and $Y(x, v)$ is a geometry dependent function for a penny shape crack emanating from hemispherical surface crack [16]:

$$Y(x/v) = 1.015 \left[A(v) + B(v) \left(\frac{x}{1+x} \right) + C(v) \left(\frac{x}{1+x} \right)^2 + D(v) \left(\frac{x}{1+x} \right)^3 \right] \quad (2)$$

with $A(v) = 1.683 + \frac{3.336}{7-5v}$, $B(v) = -1.025 - \frac{12.3}{7-5v}$, $C(v) = -1.089 + \frac{14.5}{7-5v}$, $D(v) = 1.068 - \frac{5.568}{7-5v}$.

Let us note that we do not try to calculate the lifetime of the specimen, but the number of cycles of the crack propagation period, going back from the total number of load cycles (at rupture). It was assumed that the propagation of the fatigue crack is divided in three stages so that $N_{prop} = N_{a_{int}-a_0} + N_{a_0-a_i} + N_{a_i-a}$. There is first crack initiation during $N_{a_{int}-a_0}$ cycles, from a_{int} to the crack size a_0 (a_0 corresponds to the threshold value of the stress intensity range ΔK_{th}). Then, there is the small crack propagation period $N_{a_0-a_i}$ cycles, from a_0 to the crack size a_i , and finally a long crack propagation N_{a_i-a} cycles, from a_i to the final crack size a (observed on the fracture surface of the specimen). With these three different regimes [12] the initiation regime and the quick propagation of small crack compared to long crack were considered. α is the exponent which defines the slope of the threshold curve, $da/dN = b(a/a_0)^{\alpha/2}$. The detailed equations are given in [12], they were applied to our data assuming that a_0 is corresponding to the corner for which $da/dN = b$ (in such case it means a crack propagates with a speed equal to one Burger vector per cycle, $da/dN = b$ per cycle).

Two cases are shown in Table 2 with two experimental total fatigue lives N_{exp} ; several additional cases are detailed in [12]. In the first case 99.1% of the fatigue life is due to initiation. For the second case, 96% of the fatigue life was consumed by the initiation phase. Furthermore, it has been shown in [12] that with a high value of α and large a_{int}/a_0 one obtains similar N_{Total} results than with a low α and small a_{int}/a_0 , this is because a higher α means that crack does not grow as far due to the slope of the da/dN curve in the threshold region, then a_{int}/a_0 must be larger, and with a lower α , a_{int}/a_0 must be smaller.

These calculations show that total lifetime is dominated by two phenomena: the cyclic loading assisted corrosion pitting and the crack initiation regime for creating the crack emanating from the pit. Let us recall that even if our calculations were carried out by using the crack growth curve in air, the conclusion is still valid because the crack growth rate for the R5 steel under sea water flow is higher than in air as shown in Fig. 8 and as usually reported in literature [15]. Furthermore it has to be noticed that the aim of this study is not to propose a pit growth model. Basically the aim of this study is to quantify the effect of corrosion on the VHCF strength, and to determine which phenomenon is governing corrosion fatigue under very low stress strain amplitude leading to a very high number of load cycles. Is it the corrosion process, fatigue crack initiation or propagation, or a coupling between corrosion and mechanical damage due to cyclic loading (i.e. fatigue)?

According to the authors there is actually no model that is able, in VHCF regime (that means under very low stress strain amplitudes), to model the effect of corrosion fatigue on both the

initiation of pits and the crack growth emanating from them. Additionally, there are a few studies only dealing with corrosion fatigue in metals in the very high cycle fatigue regime, most of the corrosion fatigue papers are in the low cycle fatigue regime. In that case, the phenomena are different because of macroscopic cyclic plastic strains. The aim of the crack growth calculations presented before is not to compute with a high accuracy the propagation duration of the microstructurally short crack emanating from the pit, but to assess the duration of the crack growth period including initiation, small and long crack growth. Even if the Paris–Hertzberg–Mc Clintok model [8,27,28] is not a microstructural fracture mechanics model, it takes into account with a phenomenological approach the crack growth rate differences between long crack, physically small crack and crack initiation. It has been already applied in literature to assess the crack propagation duration [9,25]. And if linear elastic fracture mechanics is not theoretically applicable for microstructurally short crack growth several empirical equations give good assessment for the key parameters of short crack growth as proposed for instance by Murakami [26].

Since previous calculations show that the fatigue life is dominated by the crack initiation regime even in corrosive environment, additional experiments have been carried out to try to understand why this initiation period is significantly affected by sea water flow.

3.4. Additional experiments and discussion about the coupling between cyclic loading and corrosion

To complete the previous tests an ultrasonic fatigue test has been carried out on a cylindrical specimen under sea water flow. Since during an ultrasonic fatigue test a stationary wave is applied on the specimen, all along this cylinder different stress amplitudes are applied at each point [17].

Fig. 10(b) shows the distribution of the stress amplitude along the cylindrical specimen loaded in its central part with a stress amplitude of 120 MPa (highest value all along the specimen). This corresponds to a mean fatigue life of 2×10^8 cycles according to the results of Fig. 4. For observation, the specimen surface was divided in 13 zones of around 1 cm long. During a single test each zone was submitted to different stress amplitudes. By testing such a cylinder under sea water flow as shown in Fig. 10(a), observation of the damaged areas allowed us to investigate the link between the stress amplitude and the damage due to the in-situ corrosion-fatigue process. The cylindrical specimen failed after 7.37×10^7 cycles.

Microscopic observations of the cylinder surface showed that R5 steel was damaged by corrosion-fatigue in the areas where the stress amplitude was higher than 56 MPa (Fig. 10(c) shows corrosion pitting in a zone loaded around 115 MPa). Few corrosion traces only was observed where the stress amplitude was smaller (Fig. 10(d)). The final fracture occurred where the stress amplitude was between 112 and 120 MPa whereas the SN curves in Fig. 4 show that below around 350 MPa without any sea water flow there

Table 2
Hemispherical surface crack growth vs. experimental fatigue life, for $x = 3$, and different a_{int}/a_0 ratios.

α	a_{int}/a_0	$N_{a_{int}-a_0}$	$N_{a_0-a_i}$	N_{a_i-a}	N_{Prop} (cycles)
Case 1: $a_0 = 9.32 \mu\text{m}$, $\sigma_a = 360 \text{ MPa}$, $R = 48 \mu\text{m}$, $a = 2.4 \text{ mm}$, $N_{exp} = 5.5 \times 10^8$ cycles on a pre-corroded specimen					
100	0.9	115,801	44,151	4,507,080	4,667,032
	0.94	13,163			4,564,394
	0.97	2,300			4,553,531
Case 2: $a_0 = 13.01 \mu\text{m}$, $\sigma_a = 200 \text{ MPa}$, $R = 290 \mu\text{m}$, $a = 2.81 \text{ mm}$, $N_{exp} = 1.08 \times 10^8$ cycles on specimen tested under sea water flow					
100	0.9	286,158	67,524	3,624,895	3,978,576
	0.94	32,528			3,724,946
	0.97	5,683			3,698,101

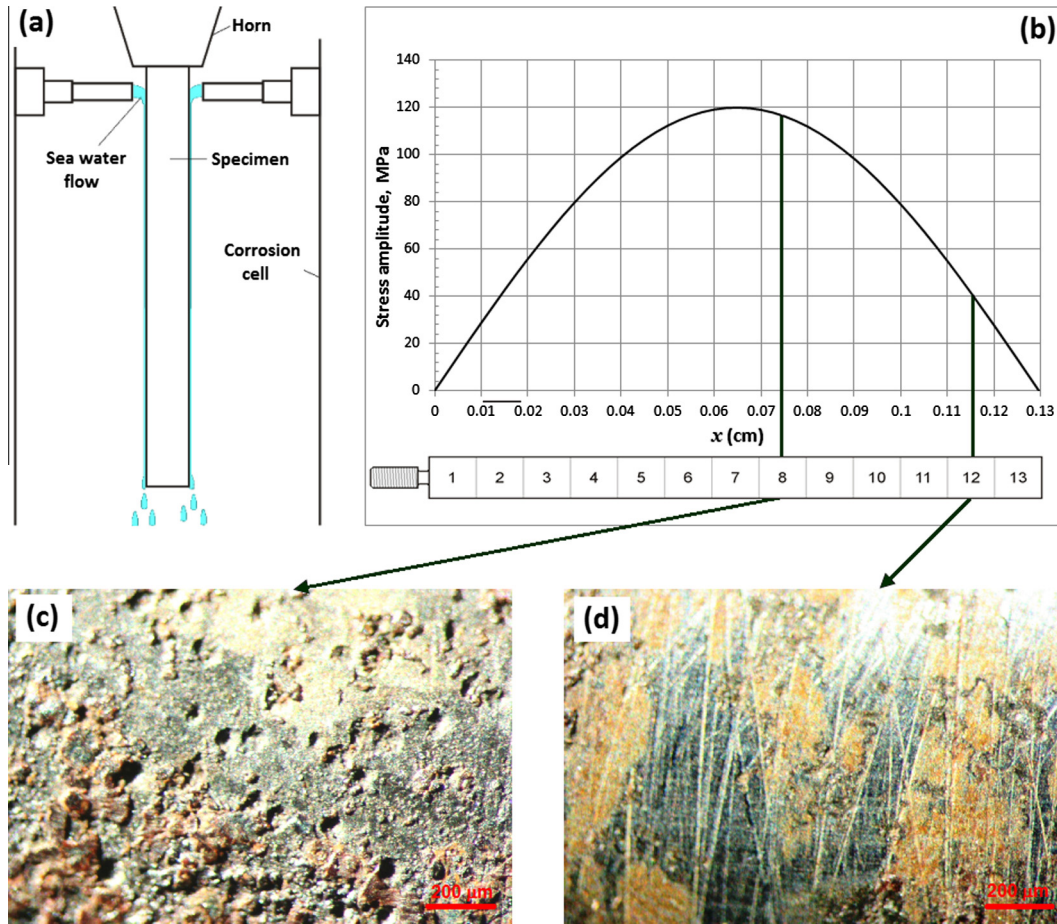


Fig. 10. (a) Schematic illustration of the test principle of a cylindrical specimen with constant cross section under sea water flow, (b) evolution of the stress amplitude along the longitudinal axis of the cylindrical specimen for a stress amplitude of 120 MPa in the central cross section, (c) and (d) optical picture of the specimen surface after 7.37×10^7 cycles in area 8 and area 12 loaded at different stress amplitudes.

was no failure after 2×10^8 cycles. This shows an experimental evidence of the strong coupling between the corrosion process and cyclic loading in a wide range of stress amplitudes even at ultrasonic frequency (20 kHz).

Furthermore, three additional tests were carried out on VHCF specimens under the same conditions than all the other tests but, without any cyclic loading. Only the sea water flow was applied on the specimen surface with the same flow rate than for the tests with cyclic loading. The aim of these tests was to quantify the corrosion damage (alone) after the same duration than 10^7 cycles (8 min 20 s at 20 kHz), 10^8 cycles (1 h 23 min 20 s at 20 kHz) and 10^9 cycles (13 h 53 min 20 s at 20 kHz). No corrosion trace was

observed by SEM after 8mn20s. After 1 h 23 min 20 s only a few traces of corrosion appear but no pits were observed. Corrosion pits were observed at the specimen surface after 13h53mn20s. The typical size of these pits was varying between 30 and 60 μm (Fig. 11) this is significantly smaller than under simultaneous cyclic loading and sea water flow (Fig. 7). The same pit size was observed under sea water flow with a stress amplitude of 240 MPa after 5×10^7 cycles. This corresponds to 42 mn only at 20 kHz! This confirms that there is a coupling between corrosion and cyclic loading.

Because of such coupling, the question of the roughness effect occurred. Complementary fatigue tests were carried out under

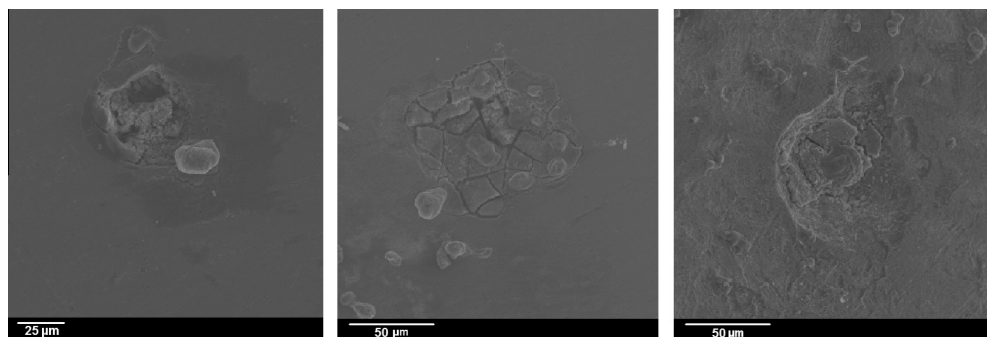


Fig. 11. Corrosion pits at the surface of a specimen under sea water flow during 13 h 53 min 20 s without any cyclic loading.

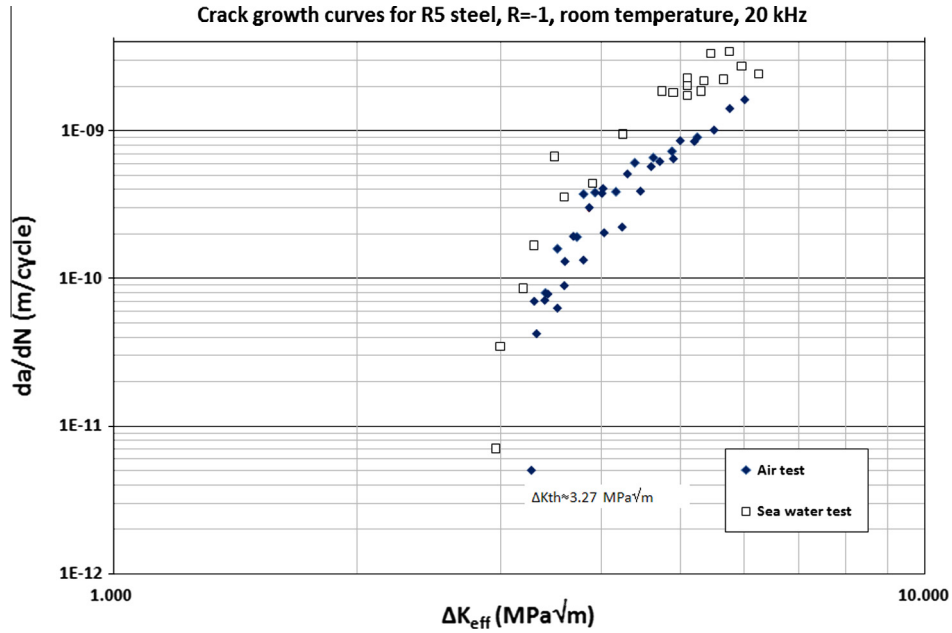


Fig. A1. Experimental $\frac{da}{dN} = f(\Delta K_{eff})$ curve in mode I for the R5 steel ($R = -1$), in air and under sea water flow at room temperature.

sea water flow at stress amplitudes between 150 and 350 MPa on the same VHCF specimens but with a polished surface ($R_a = 0.1 \mu\text{m}$) to investigate a possible roughness effect. There was no evidence of the surface roughness effect under sea water flow (Fig. 4): the fatigue results of specimens with $R_a = 0.1 \mu\text{m}$ are in the scatter band (standard deviation: 52 MPa) of the experimental data with $R_a = 0.6 \mu\text{m}$.

This study shows experimental evidence of the coupling between corrosion and mechanical damage due to cyclic stress, even at 20 kHz while some authors think that corrosion-fatigue interaction is not active when the loading frequency is high because of the long characteristic time of the corrosion process compared with the loading period. The observations of this study tend to show that the number of loading cycles or more exactly the number of reversals $2 \times N$ (not the time) is a key factor in the fatigue crack initiation phenomenon under sea water flow as suggested in [18]. We believe that when the number of reversals is high enough under a given stress amplitude, intrusions-extrusions appear at the surface of the materials. As soon as they appear there is a strong interaction with environment as suggested by Krupp [19]; consequently crack initiation is due to environmentally assisted slip irreversibility.

As some authors have reported [20] the influence of aqueous corrosive solutions on fatigue damaging is generally described in terms of surface dissolution effect or hydrogen reduction reactions (or both). Cyclic strain can enhance local electrochemical reactions which closely depend on plastic deformation [21]. In our study, working at 20 kHz in the elastic regime, plastic deformation is not present at the macroscopic scale but exists at the grain scale. The effect of dissolution occurs when fresh metal is exposed. The point at which pitting occurs at a rate less than that of crack growth is the point when mechanics becomes more dominant than electrochemical dissolution. The reason for this is that the solution chemistry is no longer favorable for dissolution at a rate that exceeds the crack growth rate. Slip irreversibility occurs because there is local plastic deformation due to the strain concentration associated with the pit stress-concentrating feature.

Further investigations should be carried out to deeply understand the physical phenomenon involved in the fatigue damage process assisted by corrosion in VHCF regime. One may imagine

ultrasonic fatigue tests with potentiostatic measurements to monitor corrosion current and potential evolution during a fatigue test. However, not immersed experiments (to avoid any cavitation) is a big experimental difficulty for carrying out such tests. Investigation of the corrosion pitting kinetics under cyclic loading is probably a key factor for a better understanding of fatigue corrosion process. In situ micro-tomography under both ultrasonic cyclic loading and sea water corrosion may be an interesting way and challenge for future researches too.

4. Conclusion and prospects

Very high cycle fatigue tests were carried out up to 10^9 cycles on smooth specimens in hot rolled martensitic-bainitic steel under three different conditions (i) virgin specimens, (ii) pre-corroded specimens and (iii) under artificial sea water flow during the fatigue test. The fatigue strength at 3×10^8 cycles is significantly reduced by a factor of 74% compared to the virgin specimens and of 71% compared to the pre-corroded ones. The poor corrosion-fatigue strength is related to the size of the pits. The assessment of the crack growth shows that crack initiation dominates the total fatigue life when $N > 10^7$ cycles. During this study a strong coupling between environment and cyclic loading has been proved. Even at ultrasonic frequency, fatigue damage and corrosion pitting are interacting for creating crack initiation at very low stress amplitude corresponding to the absence of fatigue crack initiation under fatigue in air. This has to be more investigated for understanding the physical mechanisms involved in corrosion-fatigue in VHCF regime. Anyway, it has been shown that ultrasonic fatigue tests in conjunction with sea water flowing is a good experimental way to investigate the VHCF strength of steel under corrosion conditions with reasonable test time duration.

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Appendix A

Annex 1: Experimental crack growth data (see Fig. A1).

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